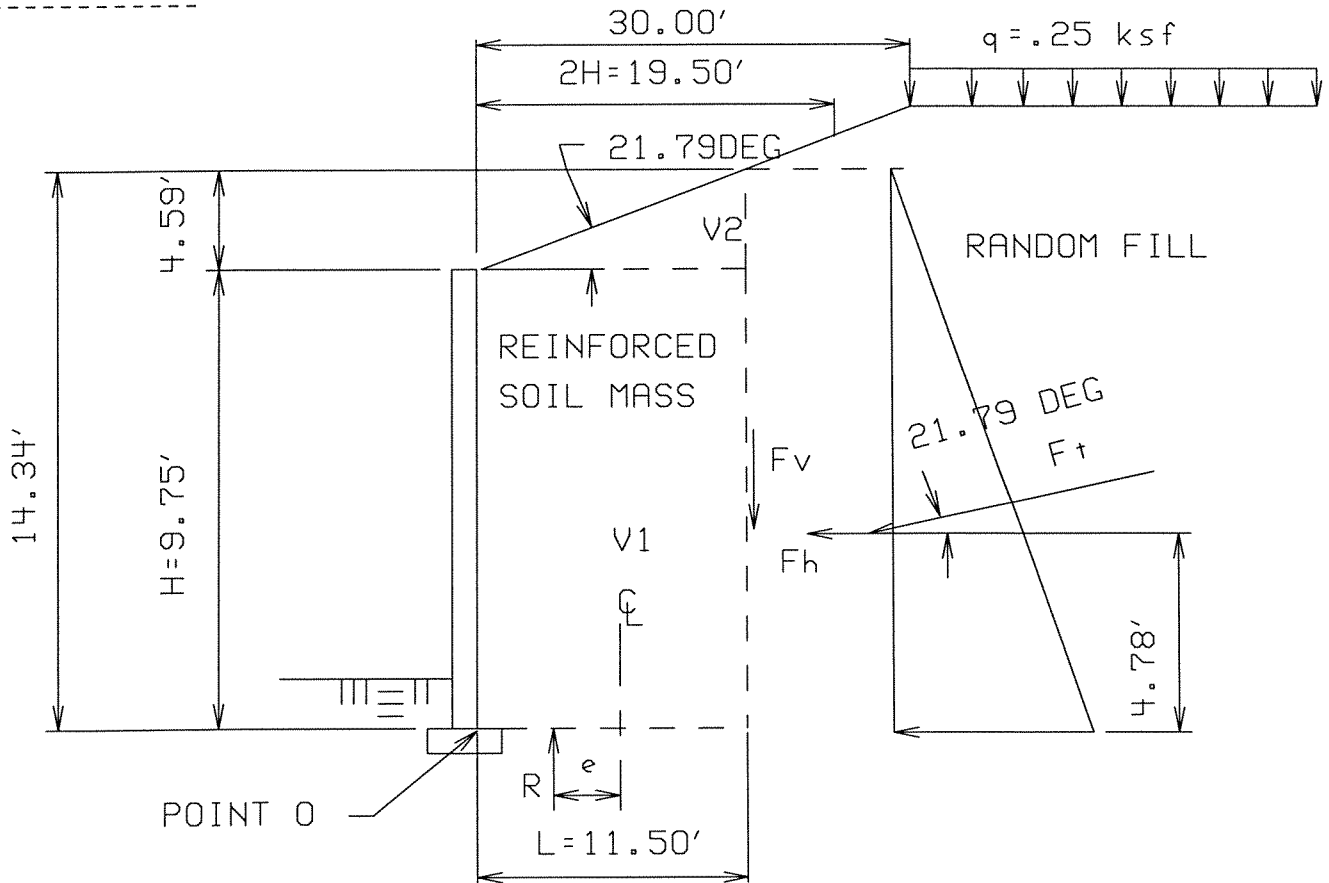


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MSE WALL DESIGN:EXISTING WALL 3N - MSE - WITH 2.5 H:1V SLOPE

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DESIGN DATA:

Design Specification: 2002 AASHTO Standard Specifications

Reinforced soil weight = 120 pcf

Random fill weight = 120 pcf

Random soil angle of internal friction,  $\phi = 30.000$  degrees

(Refer to AASHTO Figure 5.8.2C. The distance to top of slope = 30.0 ft >  $2 \cdot H = 19.5$  ft, therefore the reduced angle "I" cannot be used to compute  $K_a$ .)

Using coulomb pressure theory (see AASHTO Fig. 5.5.2A), the active coefficient of pressure to be used for horizontal component is,

$$K_a = \frac{\cos \beta \cdot \sin^2 (\theta + \phi')}{\sin^2 \theta \cdot \sin(\theta - \delta) \cdot \left| \frac{1 + [\sin(\phi' + \delta) \cdot \sin(\phi' - \beta)]}{(\sin(\theta - \delta) \cdot \sin(\theta + \beta))} \right|^{.5}} \Bigg|^2$$

$$= \frac{\cos(21.79) \cdot \sin^2 (90.00 + 30.00)}{\sin^2 (90.00) \cdot \sin(90.00 - 21.79) \cdot \left| \frac{1 - [\sin(30.00 + 21.79) \cdot \sin(30.00 - 21.79)]}{(\sin(90.00 - 21.79) \cdot \sin(90.00 + 21.79))} \right|^{.5}} \Bigg|^2$$

$$= .405$$

Also, the effects of surcharge will be ignored because the surcharge load falls outside a 1H:2V envelope measured from the back of anchorage (refer to AASHTO Fig. 5.8.12.1 for vertical surcharge distribution)

FIRM:Your Firm  
MADE BY:KJH DATE:05-13-2006  
TITLE:Example MSE wall output

JOB NO.2002-0060 SHEET NO: 2  
CHECKED BY: DATE:

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MSE WALL DESIGN:EXISTING WALL 3N - MSE - WITH 2.5 H:1V SLOPE

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DESIGN DATA (Cont'd):

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For sliding check (see '91 AASHTO Table 5.5.5B):  
Interface:Clean gravel,gravel-sand mixtures,coarse sand  
Friction factor= .550  
Adhesion = 0.000 ksf

COMPUTE WALL STABILITY (Refer to AASHTO Figure 5.8.2C):

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Equivalent fluid earth pressure = .405 \* .119 kcf = 0.048 kcf  
V1 = 11.50' \* 9.75' \* .119 kcf = 13.4 k/ft  
V2 = 0.5 \* 4.59' \* 11.50' \* .119 kcf = 3.1 k/ft  
Fh = 0.5 \* (14.34')<sup>2</sup> \* 0.048 kcf = 5.0 k/ft  
Fv = 5.0 k/ft \* Tan(21.79) = 1.9 k/ft

Safety Factor Against Overturning (Moments About Point O):

Mr = 13.4 k/ft \* 5.75' + 3.1 k/ft \* 7.66' + 1.9 k/ft \* 11.50'  
= 100.3 k\*ft/ft  
Mo = 5.0 k/ft \* 4.78 ft = 23.9 k\*ft/ft  
S.F.(O) = 100.3/ 23.9 = 4.19 > 2 (OK)

Safety Factor Against Sliding:

Fresisting = ( .550 ) \* ( 13.4 k/ft + 3.1 k/ft + 1.9 k/ft ) + 0.000 ksf \* 11.50 ft  
= 10.2 k/ft  
Fdriving = 5.0 k/ft  
S.F.(S) = 10.2/ 5.0 = 2.04 > 1.5 (OK)

Compute bearing pressure:

R = 13.4 k/ft + 3.1 k/ft + 1.9 k/ft = 18.6 k/ft  
e = L/2 - (Mr - Mo)/R  
= 11.50'/2 - ( 100.3 k\*ft/ft - 23.9 k\*ft/ft ) / 18.6 k/ft  
= 1.64 < L/6 = 11.50'/6 = 1.91' (OK)

The width of soil pressure in bearing is,

L - 2\*e = 11.50 ft - 2\*( 1.64 ft )  
= 8.20 ft

Bearing pressure,  $\sigma_v$  = R/(L - 2\*e)  
= 18.62/(11.50 - 2\*1.64)  
= 2.269 ksf